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Some physico-chemical and radiation properties of plutonium-238 metal prepared by electrochemical amalgamation

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Abstract

Pu-238 metal was prepared by electrolytic amalgamation from Pu(III) acetate aqueous solution and by followed by the thermal decomposition of the Pu amalgam. The density, specific heat power, γ -spectra, neutron flux, and corrosion kinetics in dry air at ambient temperature of the prepared ²³⁸Pu metal were measured. The neutron flux and γ -spectra from ²³⁸Pu metal have been attributed to spontaneous and induced fission and to $(\alpha, \alpha' \gamma)$, $(\alpha, p\gamma)$, and $(\alpha, n\gamma)$ nuclear reactions on light nuclei. The electrochemically prepared ²³⁸Pu metal was shown to generate fewer neutrons, produce less gamma radiation, and contains lower ¹⁰B, ¹⁹F, and ²⁸Si impurities in comparison with biomedical ²³⁸PuO₂. The increase of neutron flux from the sample due to the reaction ¹⁸O($\alpha, n\gamma$) ²¹Ne was shown to be proportional to the increase of the mass of the ²³⁸Pu metal with time due to corrosion in dry air. ²³⁸Pu metal corrosion rate maximum and average values (1.1×10^{-2} and 4.7×10^{-3} mg cm⁻² h⁻¹, respectively) obtained in dry air were an order of magnitude higher than the rates published for ²³⁹Pu under similar experiment conditions. The difference between the ²³⁹Pu and ²³⁸Pu metal corrosion rate and mechanism is proposed to be due to the greater radiation effects and temperature on the ²³⁸Pu surface. © 2007 Elsevier B.V. All rights reserved.

Keywords: ²³⁸Pu; Metal; Corrosion; $(\alpha, n\gamma)$ reactions

1. Introduction

²³⁸Pu is widely applied as a power source in cardiac pacemakers (each using ~160 mg ²³⁸Pu) and in remote power generation (e.g., the Apollo spaceships contained 14 kg ²³⁸Pu for its power generators [1]). The ²³⁸Pu generally is present as ²³⁸PuO₂ with natural oxygen or with oxygen depleted in ¹⁷O and ¹⁸O to reduce neutron yields from (α,n) reactions [2]. The properties of ²³⁸Pu metal are studied in less details than those of ²³⁹Pu metal. The goal of this work is to study some properties of ²³⁸Pu metal prepared by the non-conventional method of electrochemical amalgamation from Pu(III) aqueous solution and subsequent thermal decomposition of the plutonium amalgam [3]. The primary research focus is on ²³⁸Pu metal pellet corrosion in air and to the increase of neutron flux and γ-radiation from the pellet arising due to the formation of ²³⁸PuO₂ and the nuclear reactions

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¹⁸O(α,nγ)²¹Ne and ¹⁸O(α,α'γ)¹⁸O. Despite data from numerous studies of ²³⁹Pu metal corrosion [3–5], analogous data for ²³⁸Pu are, for us, inaccessible or absent. The corrosion rates of ²³⁸Pu and ²³⁹Pu metals are expected to differ because of the higher specific α-activity of ²³⁸Pu metal.

2. Experimental

The plutonium used in this testing, purified of its daughter uranium, had the isotope composition, determined by mass-spectrometry, as given in Table 1. The reduction of Pu(III) to the intermetallic compounds Pu(Hg)_n, where $0 \le n \le 4$ (up to 0.5–0.6 kg Pu per liter Hg), was made by electrolytic amalgamation of 0.08 M Pu(III) in 1 M acetate buffer solution (pH 3.5–4.5) at (0.90–1.2)·10³ A/m² current density at a Hg cathode at 10–15 °C. The plutonium was isolated from the amalgam by its thermal decomposition. The mercury was swept from the plutonium by an argon stream at 600 °C; removal of residual Hg and trace sodium occurred at vacuum melting at 1100 °C. A more detailed description of ²³⁸Pu metal preparation by electrolytic amalgamation is given in [3]. The obtained plutonium ingots were pressed at 4.5–7.5 kbar under an air atmosphere to prepare cylindrical pellets of 5 mm diameter and 2–4 mm height. The plutonium metal pellet corrosion experiments were carried out in boxes with 25 ± 3 °C air atmosphere at 30% relative humidity. The photon flux from the prepared Pu pellets and from biomedical-quality ²³⁸PuO₂ were measured in the energy region

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^{80.0} Г

Table 1Isotope composition of studied plutonium

Isotope	Content (mass%)	
²³⁸ Pu	80.7	
²³⁹ Pu	16.0	
²⁴⁰ Pu	2.7	
²⁴¹ Pu	0.6	

0.1–1.5 MeV without filter and in 1.1–3.0 MeV with a 20 mm lead and 3 mm iron filter. The fast neutron fluxes of the prepared ²³⁸Pu metal pellets were measured using the Russian model UNS neutron coincidence counter. Standard sources of biomedical ²³⁸PuO₂ were used for counter calibration. Summary inaccuracy of neutron flux measurements was lower 5%.

3. Results and discussion

3.1. Some physical properties of prepared ²³⁸Pu metal

The densities of the pellets samples prepared by pressing of plutonium ingots were calculated after the measuring of their masses and the geometrical sizes. The densities were found to depend weakly on the preparation pressure in the studied 4.5-7.5 kbar interval, and their values varied from 16.1 to 17.0 g cm⁻³. Prepared ²³⁸Pu metal was supposed to crystallize in alpha-phase at ambient temperature and obtained densities were about 81–85% of the density of α -²³⁹Pu measured by Xray diffraction technique at the same conditions. The thermal power was found by calorimetry to be 0.45 W/g for the studied Pu samples. The results of γ -spectra measurements from prepared ²³⁸Pu metal and from biomedical ²³⁸PuO₂ are given in Table 2. The identification of the nuclear reactions and light nuclei impurities were done by their photon energy using published data [6,7]. The data of Table 2 show that no radioactive impurities were present in either the biomedical ²³⁸PuO₂ or in the ²³⁸Pu metal. Stable light-element impurities of F, B, and Si were detected by gamma analysis in ²³⁸PuO₂ samples but no impurities were found by gamma analysis of the ²³⁸Pu metal samples. This indicates that proposed electrochemical method of Pu metal preparation provides high purification of plutonium from light impurities and hence provides a lower level of photon and neutron irradiation from Pu metal in comparison with biomedical ²³⁸PuO₂.

Table 2

Gamma-spectrometric determination of light nuclei impurities in biomedical ²³⁸PuO₂ and in ²³⁸Pu metal prepared by electrochemical amalgamation

60.0 - I E € 40.0 - Z 20.0 - 20.0 -		,	 - -	5.0 4.0 3.0 <i>X</i> 2.0 1.0 0.0
0.0 0 500	1000	1500	200	-1.0 ⁰⁰ •?m
	time, h			— □ — ? N

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Fig. 1. Mass sample and neutron flux increase during 238 Pu metal corrosion in air at 25 °C. Mass sample 1.1 g, S = 0.82 cm², air humidity 30%. I, II and III—the stages of the corrosion process.

Table 3	
²³⁸ Pu metal corrosion rate at different stage in dry air	

Interval (h)	Corrosion rate (mg Pu/cm ² min)
(I) 0–700 (II) 700–1350	Non detected 1.1×10^{-2}
(III) 1350–1820	3.3×10^{-3}
Average corrosion rate, 0–1820	4.8×10^{-3}

3.2. ²³⁸*Pu metal corrosion in air and the increase of neutron flux from the sample*

The corrosion rate of ²³⁸Pu metal was determined by measuring the sample mass increase and the neutron flux increase as function of time. The parameters were found to be proportional and changed in the same manner during the experiment time. The mass sample increase in dry air due to combination with oxygen and the reaction ¹⁸O(α ,n γ)²¹Ne (Fig. 1) demonstrate the kinetics of ²³⁸Pu metal corrosion. Three separate corrosion stages (steps) could be marked. The corrosion rates, calculated from the Fig. 1 data for each stage, are given in Table 3. Comparison of rate values from Table 3 with published data shows that ²³⁸Pu metal corrodes in 25 °C air about 10-times more rapidly than does

Sample	Detected photon energy (keV)	Measured photon intensity, photon/s g ²³⁸ Pu	Detection limit for photon of this energy, photon/s g ²³⁸ Pu	Nuclear reaction ^a
Biomedical ²³⁸ PuO ₂	1236	$(4.2 \pm 0.6)1 \times 0^3$	170	$^{19}F(\alpha, \alpha'\gamma)^{19}F$
	1275	$(1.1 \pm 0.2) \times 10^4$	170	$^{19}F(\alpha,p\gamma)^{22}Ne$
	1395	$(2.0\pm0.6)\times10^3$	250	$^{18}O(\alpha,n\gamma)^{21}Ne$
	1528	$(1.1 \pm 0.6) \times 10^3$	190	$^{19}F(\alpha,n\gamma)^{22}Na$
	1632	$(2.5 \pm 0.6) \times 10^3$	240	${}^{10}B(\alpha,\alpha'\gamma){}^{10}B$
	1779	$(1.3 \pm 0.6) \times 10^3$	300	28 Si($\alpha, \alpha' \gamma$) 28 Si
	1982	$(1.6 \pm 0.6) \times 10^3$	340	$^{18}O(\alpha, \alpha'\gamma)^{18}O$
	2081	$(4.4 \pm 0.6) \times 10^3$	470	$^{19}F(\alpha,p\gamma)^{22}Ne$
	2234	$(2.7 \pm 0.6) \times 10^3$	600	28 Si(α ,p γ) 31 P
²³⁸ Pu metal	None found	_	_	_

^a The identification of the light nuclei was done using data [6,7].

6.0

Kinetic parameters of ²³⁸ Pu metal oxidation in air ^a at 25 °C				
Determination method	Measured parameters	Stage 2	Stage 3	
Measurement of mass increase	$k_{\rm eff.} ({\rm mg}{\rm Pu}{\rm cm}^{-2}{\rm h}^{-1})$	$(3.1 \pm 1.8) \times 10^{-3}$	$(2.7 \pm 0.99) \times 10^{-4}$	
Neutron flux measurement	$n = k_{\rm eff.} ({\rm mg Pu cm^{-2} h^{-1}})$	$4.10 \pm 0.15 (2.7 \pm 1.9) \times 10^{-3}$	1.00 ± 0.04 $(2.4 \pm 0.8) \times 10^{-4}$	

п

Table 4 Kinetic parameters of ²³⁸Pu metal oxidation in air^a at 25 °C

^a Air humidity was 30%, mass sample 1.1 g



Fig. 2. 238 Pu metal corrosion kinetics in air at 25 °C in logarithmic coordinates. Sample mass 1.1 g, 30% relative humidity air.

²³⁹Pu (10⁻⁴ to 10⁻³ mg cm⁻² h⁻¹ [4,5]) under similar closed conditions. The difference in corrosion rates between ²³⁸Pu and ²³⁹Pu is likely caused by the higher specific activity of ²³⁸Pu, which is 275-times greater than that of ²³⁹Pu [6], to produce higher surface temperature and greater radiolytic decomposition of adsorbed water vapor film on the ²³⁸Pu metal surface. It is important to note that the ~1 g ²³⁸Pu metal sample in an open glass tube did not show visible corrosion, weight gain, or increased neutron radiation during the first 30 days in 25 °C air at 30% humidity. Alloying with Ga, Zr, or other metals with Z > 20 is necessary to obtain better corrosion stability of ²³⁸Pu.

The corrosion mechanism developed for ²³⁹Pu [4,5] includes the formation of intermediate products Pu₂O₃ and PuH₃ before the final product PuO₂. This mechanism can be accepted for ²³⁸Pu with some additions. The first step (\approx 30 days) is latent slow corrosion during which no increase of sample mass or neutron flux is detected. Water vapor adsorption on the metal surface and the formation of initial corrosion centers (embryo), containing Pu₂O₃ and PuH₃, occurs during the first latent stage. The corrosion rate increases quickly at the second stage, which continues \approx 30 days and gives ²³⁸PuO₂ as the main product. The third stage is characterized by some corrosion rate diminution due to the formation of a thick passive ²³⁸PuO₂ film, which hinders diffusion of oxygen and water vapor to the plutonium metal surface. The logarithmic analysis of corrosion kinetic curves on the stages 2 and 3 shows (Fig. 2) that the process can be described by the following equation:

 0.96 ± 0.05

 4.15 ± 0.12

$$k_{\rm eff}t^n = \frac{\mathrm{d}(m_t m_{\rm o}/m_{\rm o})}{\mathrm{d}t} \tag{1}$$

where k_{eff} is the effective constant of ²³⁸Pu metal corrosion rate, n in an empirical exponent dependent on surface changes and the active reagent diffusion rate through the surface. The values k_{eff} and n obtained by measuring mass increase and by neutron flux increase are given in Table 4. Plutonium nitride formation, which is negligible during ²³⁹Pu corrosion in air, becomes more probable as a ²³⁸Pu metal intermediate corrosion product because the Pu atoms and N₂ molecules receive more excitation energy due to alpha-radiolysis and recoil phenomenon on the ²³⁸Pu surface than in the case of ²³⁹Pu.

4. Conclusions

- 1. The ²³⁸Pu metal prepared from aqueous solution by the electrochemical amalgamation method contains lower concentrations of light nuclei B, F, and Si impurities than standard biomedical ²³⁸PuO₂ to produce significantly less photon and neutron radiation due to $(\alpha,n\gamma)$ reactions.
- 2. The ²³⁸Pu metal corrosion rate, measured in air by the increase of ²³⁸Pu metal mass sample and by the increase of neutron flux from the sample, was found to be order of magnitude higher than that of ²³⁹Pu metal at similar conditions.

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